

IN THE CLAIMS:

1. A method for ~~differentiating if~~ detecting collisions ~~a feedback signal is a result of an unintentional collision in a servo system, between an obstacle and an electromechanical system having a mechanical output controlled by a servo system,~~ said method ~~comprising~~ comprising:

inputting a forcing function  $x_i$  to the servo system to direct the mechanical output to move in an intended manner;

generating a difference signal at a monitoring point M representing a difference between forcing function  $x_i$  and a feedback signal dependent upon the mechanical output;

injecting a feed forward ~~term in the servo system.~~ signal into the servo system, said feed forward signal dependent upon the forcing function and effective to increase a detection threshold for collision stimulus at monitoring point M; and

processing said difference signal to detect a collision.

2. (cancelled)

3. (cancelled)

4. (currently amended) A method in accordance with ~~Claim 1~~ Claim 21 ~~further comprising optimizing wherein said optimizing transfer function  $y_0/x_2$  comprises optimizing  $y_0/x_2$  without the influence of the feed forward signal. forward, wherein  $x_2$  is a load function and  $y_0$  is an output of the servo system.~~

5. (cancelled)

6. (cancelled)

7. (currently amended) An imaging system comprising:

a radiation source;

a radiation detector positioned to receive radiation emitted by said source;

a servo system configured to position at least one of said source, said detector, and an object to be scanned; and

said imaging system configured to input a forcing function  $x_i$  to the servo system to direct at least one of said source, said detector, and said object to be scanned to move in an intended manner; generate a difference signal at a monitoring point M representing a difference between forcing function  $x_i$  and a feedback signal dependent upon a mechanical output; injecting a feed forward signal in said servo system, said feed forward signal dependent upon the forcing function and effective to increase a detection threshold for collision stimulus at monitoring point M; and process said difference signal to detect a collision.

~~a computer operationally coupled to said source, said detector, and said servo system, said computer configured to inject a feed forward term in said servo system.~~

8. (cancelled)

9. (cancelled)

10. (cancelled)

11. (cancelled)

12. (currently amended) A system in accordance with ~~Claim 9~~ Claim 32 wherein said computer further configured to optimize  $y_o/x_2$  without the influence of the feed forward signal. forward, wherein  $x_2$  is a load function.

13. (cancelled)

14. (cancelled)

15. (cancelled)

16. (cancelled)

17. (cancelled)

18. (cancelled)

19. (currently amended) A method of ~~configuring~~ operating a servo system ~~with~~ having an initial aggressiveness level for responding to a collision and a desired aggressiveness level for responding to an input control signal, said method comprising:

reducing the initial aggressiveness level for responding ~~to a~~ to the collision;  
and

maintaining the desired aggressiveness level for responding to the input.

20. (original) A method in accordance with Claim 19 wherein the servo system includes a feedback system, said reducing the initial aggressiveness level comprises reducing the initial aggressiveness level by optimizing the feedback system for collisions.

21. (original) A method in accordance with Claim 20 wherein said maintaining the desired aggressiveness level for responding to the input comprises maintaining the desired aggressiveness level for responding to the input by providing a feed forward term to the servo system.

22. (new) A method in accordance with Claim 1 further comprising optimizing a transfer function  $y_o/x_2$ , wherein  $y_o$  is a signal representative of the mechanical output and  $x_2$  is a load function.

23. (new) A method in accordance with Claim 22 wherein said feed forward signal dependent upon the forcing function is selected to also optimize a transfer function  $y_o/x_i$ .

24. (new) A method in accordance with Claim 21 wherein said feed forward signal is injected into a plurality of points in the servo system.

25. (new) A method in accordance with Claim 1 further comprising initiating a command to stop movement when a collision is detected.

26. (new) An apparatus comprising:

a servo system;

an electromechanical system having a mechanical output controlled by said servo system;

said servo system configured to input a forcing function  $x_i$  to the servo system to direct the mechanical output to move in an intended manner, generate a difference signal at a monitoring point M representing a difference between forcing function  $x_i$  and a feedback signal dependent upon said mechanical output, and inject a feed forward signal into the servo system, said feed forward signal dependent upon the forcing function and effective to increase a detection threshold for collision stimulus at monitoring point M; and

said apparatus further configured to process said difference signal to detect a collision.

27. (new) An apparatus in accordance with Claim 26 further configured to optimize a transfer function  $y_o/x_2$  of the servo system, wherein  $y_o$  is signal representative of said mechanical output and  $x_2$  is a load function.

28. (new) An apparatus in accordance with Claim 27 wherein said feed forward signal dependent upon the forcing function is selected to also optimize a transfer function  $y_o/x_i$ .

29. (new) An apparatus in accordance with Claim 27 wherein  $y_o/x_2$  is optimized without the influence of the feed forward signal.

30. (new) An apparatus in accordance with Claim 26 configured to inject said feed forward signal into a plurality of points in said servo system.

31. (new) An apparatus in accordance with Claim 26 further configured to initiate a command to stop movement when a collision is detected.

32. (new) A system in accordance with Claim 7 further configured to optimize a transfer function  $y_o/x_2$  of the servo system, wherein  $y_o$  is signal representative of said mechanical output and  $x_2$  is a load function.

33. (new) A system in accordance with Claim 32 wherein said feed forward signal dependent upon the forcing function is selected to also optimize a transfer function  $y_o/x_i$ .

34. (new) A system in accordance with Claim 7 configured to inject said feed forward signal into a plurality of points in said servo system.

35. (new) A system in accordance with Claim 7 further configured to initiate a command to stop movement when a collision is detected.

IN THE ABSTRACT:

*Please replace the Abstract on Page 18 of the originally filed Application with the Abstract on the separate page attached to this Amendment. For convenience, a copy of the new Abstract showing the changes introduced by this replacement is provided below.*

A method for ~~differentiating if a feedback signal is a result of an unintentional collision in a servo system includes~~ detecting collisions between an obstacle and an electromechanical system having a mechanical output controlled by a servo system includes inputting a forcing function  $x_i$  to the servo system to direct the mechanical output to move in an intended manner. A difference signal is generated at a monitoring point M representing a difference between forcing function  $x_i$  and a feedback signal dependent upon the mechanical output. The method further includes injecting a feed forward ~~term in~~ signal into the servo system. The feed forward signal is dependent upon the forcing function and effective to increase a detection threshold for collision stimulus at monitoring point M. The method also includes processing the difference signal to detect a collision.

A method for detecting collisions between an obstacle and an electromechanical system having a mechanical output controlled by a servo system includes inputting a forcing function  $x_i$  to the servo system to direct the mechanical output to move in an intended manner. A difference signal is generated at a monitoring point M representing a difference between forcing function  $x_i$  and a feedback signal dependent upon the mechanical output. The method further includes injecting a feed forward signal into the servo system. The feed forward signal is dependent upon the forcing function and effective to increase a detection threshold for collision stimulus at monitoring point M. The method also includes processing the difference signal to detect a collision.

IN THE SPECIFICATION:

*Note: In the following replacements, tables and equations appearing on separate lines are considered to be part of the last-numbered paragraph above the table or equations if the tables or equations are not denoted by a separate paragraph number in brackets in the original specification. Therefore, these tables and equations are reproduced in the substitution paragraphs below even if no changes are to be made within the tables and equations.*

*Because of the difficulty of using the standard typographical conventions of underlining, strikethrough, and double brackets for indicating amendments to tables and equations and the probable confusion that would result, any amendments to tables or equations are specifically cited in the italicized notes above the paragraphs rather than indicated by these typographical conventions.*

*Please replace paragraph [0028] of the specification with the following amended paragraph of the same number:*

[0028]  $G_1$  can be chosen to make  $y_o/x_2$  behave optimally for collision detection and avoidance. An alternative version of  $G_1$  is selected and defined as  $G_1'$ , which is chosen to ~~make  $y_o/x_i$  behave~~ make  $y_o/x_2$  behave optimally from the point of view of the forcing function  $x_i$  but without using feed forward ( $F_1 = 0$ ). The alternative versions for  $G_1$  and  $G_1'$  are indicated as option 1 and option 2 in Figure 3, where, in option 1,  $F_2=1$  and in option 2,  $F_1=0$ . Finally, using  $G_1$  and  $F_1$  (but not  $G_1'$ ), require a transfer function ~~for  $y_o/x_i$  that~~ for  $y_o/x_2$  that behaves identically to the prior  $y_o/x_i$ , and solve for the required  $F_1$  to force this result. The following equations show this process.

$$2) \frac{(F_1 + 1)G_1 G_2}{1 + G_1 G_2 H} = \frac{G_1' G_2}{1 + G_1' G_2 H}$$

Solving for  $F_1$ :

$$3) F_1 = \frac{G_1'(1 + G_1 G_2 H) - G_1(1 + G_1' G_2 H)}{G_1(1 + G_1' G_2 H)}$$



Please replace paragraph [0030] of the specification with the following amended paragraph of the same numbers, further noting that each and every occurrence of the variable "F" inside equation 4) is changed to "F<sub>1</sub>" (there were no occurrences of "F<sub>1</sub>" in these equations as originally filed):

[0030] Figure 4 illustrates a specific example of an electromechanical servos system shown generically in Figure 3. In Figure 4, K<sub>count</sub> is motor amplifier gain. K<sub>3</sub>/s is quadrature rotary gain (with N slits), K<sub>m</sub> corrects gain applied to the output via a lead screw. K<sub>1</sub>, K<sub>2</sub>, and P<sub>2</sub> are motor parameters. Other values are chosen with programming. The closed loop response for Figure 4 inputs x<sub>1</sub> and x<sub>2</sub> are given

$$4) y_0 = x_1 \frac{(F_1 + 1) \frac{K_2 K_3 K_5}{Z_5 Z_6} s^2 + (F_1 + 1) \left( \frac{1}{Z_5} + \frac{1}{Z_6} \right) K_2 K_3 K_5 s + (F_1 + 1) K_2 K_3 K_5}{\frac{1}{P_2 P_6} s^4 + \left( \frac{1}{P_2} + \frac{1}{P_6} \right) s^3 + \left( \frac{K_2 K_3 K_4 K_5}{Z_5 Z_6} + 1 \right) s^2 + \left( \frac{1}{Z_5} + \frac{1}{Z_6} \right) K_2 K_3 K_4 K_5 s + K_2 K_3 K_4 K_5}$$

$$- x_2 \frac{\frac{K_1 K_3}{P_6} s^2 + K_1 K_3 s}{\frac{1}{P_2 P_6} s^4 + \left( \frac{1}{P_2} + \frac{1}{P_6} \right) s^3 + \left( \frac{K_2 K_3 K_4 K_5}{Z_5 Z_6} + 1 \right) s^2 + \left( \frac{1}{Z_5} + \frac{1}{Z_6} \right) K_2 K_3 K_4 K_5 s + K_2 K_3 K_4 K_5}$$

Please replace paragraph [0031] of the specification with the following amended paragraph of the same numbers, further noting that each and every occurrence of the variable "F" inside equations 7), 8), 9), and 10) is changed to "F<sub>1</sub>" (there were no occurrences of "F<sub>1</sub>" in these equations as originally filed):

[0031] Next, for y<sub>0</sub>/x<sub>i</sub> preferred terms K'<sub>5</sub> and Z'<sub>5</sub> are selected instead of K<sub>5</sub> and Z<sub>5</sub>. ~~With no feed forward (F=0) this result in:~~ With no feed forward (F<sub>1</sub>=0), this results in:

$$5) \frac{y_0}{x_i} = \frac{\frac{K_2 K_3 K'_5}{Z'_5 Z_6} s^2 + \left( \frac{K'_5}{Z'_5} + \frac{K'_5}{Z_6} \right) K_2 K_3 s + K_2 K_3 K'_5}{\frac{1}{P_2 P_6} s^4 + \left( \frac{1}{P_2} + \frac{1}{P_6} \right) s^3 + \left( \frac{K_2 K_3 K_4 K'_5}{Z'_5 Z_6} + 1 \right) s^2 + \left( \frac{1}{Z'_5} + \frac{1}{Z_6} \right) K_2 K_3 K_4 K'_5 s + K_2 K_3 K_4 K'_5}$$

From inspection of Figure 4 it is clear that

$$6) M = x_i - y_0 K_4$$

~~F can be determined~~ F<sub>1</sub> can be determined using equation 3) to obtain equation 7).

$$7) F_1 = \frac{K'_5 \times \frac{\frac{s}{Z'_5} + 1}{s} \times \frac{\frac{s}{Z_6} + 1}{\frac{s}{P_6} + 1} \times K_2 \times \left( 1 + K_5 \times \frac{\frac{s}{Z'_5} + 1}{s} \times \frac{\frac{s}{Z_6} + 1}{\frac{s}{P_6} + 1} \times K_2 \times \frac{1}{\frac{s}{P_2} + 1} \times \frac{K_3}{s} \times K_4 \right) - K_5 \times \frac{\frac{s}{Z'_5} + 1}{s} \times \frac{\frac{s}{Z_6} + 1}{\frac{s}{P_6} + 1} \times K_2 \times \left( 1 + K'_5 \times \frac{\frac{s}{Z'_5} + 1}{s} \times \frac{\frac{s}{Z_6} + 1}{\frac{s}{P_6} + 1} \times K_2 \times \frac{1}{\frac{s}{P_2} + 1} \times \frac{K_3}{s} \times K_4 \right)}{K_5 \times \frac{\frac{s}{Z'_5} + 1}{s} \times \frac{\frac{s}{Z_6} + 1}{\frac{s}{P_6} + 1} \times K_2 \times \left( 1 + K'_5 \times \frac{\frac{s}{Z'_5} + 1}{s} \times \frac{\frac{s}{Z_6} + 1}{\frac{s}{P_6} + 1} \times K_2 \times \frac{1}{\frac{s}{P_2} + 1} \times \frac{K_3}{s} \times K_4 \right)}$$

Rearranging equation 7), one obtains 8)

$$8) F_1 = \frac{\left( \frac{K_2 K'_5}{Z'_5 Z_6} s^2 + \left( \frac{1}{Z'_5} + \frac{1}{Z_6} \right) K_2 K'_5 s + K_2 K'_5 \right) \left( \frac{1}{P_2 P_6} s^4 + \left( \frac{1}{P_2} + \frac{1}{P_6} \right) s^3 + \left( \frac{K_2 K_3 K_4 K'_5}{Z'_5 Z_6} + 1 \right) s^2 + \left( \frac{1}{Z'_5} + \frac{1}{Z_6} \right) K_2 K_3 K_4 K'_5 s + K_2 K_3 K_4 K'_5 \right) - \left( \frac{K_2 K_5}{Z'_5 Z_6} s^2 + \left( \frac{1}{Z'_5} + \frac{1}{Z_6} \right) K_2 K_5 s + K_2 K_5 \right) \left( \frac{1}{P_2 P_6} s^4 + \left( \frac{1}{P_2} + \frac{1}{P_6} \right) s^3 + \left( \frac{K_2 K_3 K_4 K'_5}{Z'_5 Z_6} + 1 \right) s^2 + \left( \frac{1}{Z'_5} + \frac{1}{Z_6} \right) K_2 K_3 K_4 K'_5 s + K_2 K_3 K_4 K'_5 \right)}{\left( \frac{K_2 K_5}{Z'_5 Z_6} s^2 + \left( \frac{1}{Z'_5} + \frac{1}{Z_6} \right) K_2 K_5 s + K_2 K_5 \right) \left( \frac{1}{P_2 P_6} s^4 + \left( \frac{1}{P_2} + \frac{1}{P_6} \right) s^3 + \left( \frac{K_2 K_3 K_4 K'_5}{Z'_5 Z_6} + 1 \right) s^2 + \left( \frac{1}{Z'_5} + \frac{1}{Z_6} \right) K_2 K_3 K_4 K'_5 s + K_2 K_3 K_4 K'_5 \right)}$$

For simplification, a change of notation is used, referencing equation 8).

$$9) F_1 = \frac{(As^2 + Bs + C)(Ds^4 + Es^3 + Ps^2 + Gs + H) - (Is^2 + Js + K)(Ds^4 + Es^3 + Ls^2 + Ms + N)}{(Is^2 + Js + K)(Ds^4 + Es^3 + Ls^2 + Ms + N)}$$

Finally,

$$10) F_1 = \frac{(AD-ID)s^6 + (AE+BD-IE-JD)s^5 + (AP+BE+CD-IL-JE-KD)s^4 + (AG+BP+CE-IM-JL-KE)s^3 + (AH+BG+CP-IN-JM-KL)s^2 + (BH+CG-JN-KM)s + CH-KN}{ID s^6 + (IE+JD)s^5 + (IL+JE+KD)s^4 + (IM+JL+KE)s^3 + (IN+JM+KL)s^2 + (JN+KM)s + KN}$$

*Please replace paragraph [0032] of the specification with the following amended paragraph of the same numbers:*

[0032] For the example application, the loop gain Bode plot that is optimized for  $x_i$  is given in Figure 5 with associated optimized parameters listed in Table 1. Note, the loop gain Bode plot in Figure 5 was optimized for  $x_i$  using  $K_5'$  and  $Z_5'$ . Because of the feed forward ~~parameter F~~ parameter  $F_1$  (equation 10), this plot's phase margin can be used to predict the transient response of  $y_o/x_i$ . Note that for true stability, a Bode plot using  $K_5$  and  $Z_5$  (not  $K_5'$  and  $Z_5'$ ) can be used.

System Parameters	Servo Inputs	Calculations
Kcomp = 0.07		Tm = 0.086
K4 = 1		K5' = 0.0060 20
Z5' = 5		P2 = 11.655
Tsample period = 0.002		Z6 = 11.656
Tcomp time = 0.002		K2 = 41.841
w start = 0.1		K1 = 2626.0 04
Scale Factor = 1.2		K3 = 318.31 0
Quad Enc Slits = 500		Km = 1.000
R = 1.5		Kloop@1r = 80.177
Ke = 0.0239		
J = 3.27E-05		
Kcount = 0.086		
Kleadscrew = 318.31		

Table 1

*Please replace paragraph [0034] of the specification with the following amended paragraph of the same numbers:*

[0034] For an actual system represented by the example application, some blocks of Figure 4 (including ~~the F-term~~ the  $F_1$ -term given in equation 10) could be implemented in a computer and those functions accomplished via software programming using z-transforms of the Laplace equations. Other parts of the system can be realized in the form of electronic circuitry, an electric motor, and mechanical drive parts and other physical mechanisms. By proper use of equations 4), 5), and 6) a simulation of responses for the example application can be obtained, as though the feed forward term defined in equation 10) had been applied to an actual servo system.